

Designing a 500 kVA, 60Hz, K-Factor, three phase dry transformer with cooling channels?

General Information

Technical Specification

Input voltage	3 x 480V, delta
Output voltage	3 x 208/120V, star
Output power	500kVA, K-Factor=20, continuous operating mode
Frequency	60Hz
Ambient temperature	40°C, in a cabinet
Temperature rise	Max. 120°K, insulation class H
°Short-circuit voltage	4-5%
Steel&core	M6, not annealed, strips for alternated stacking (90°)

Creating Input

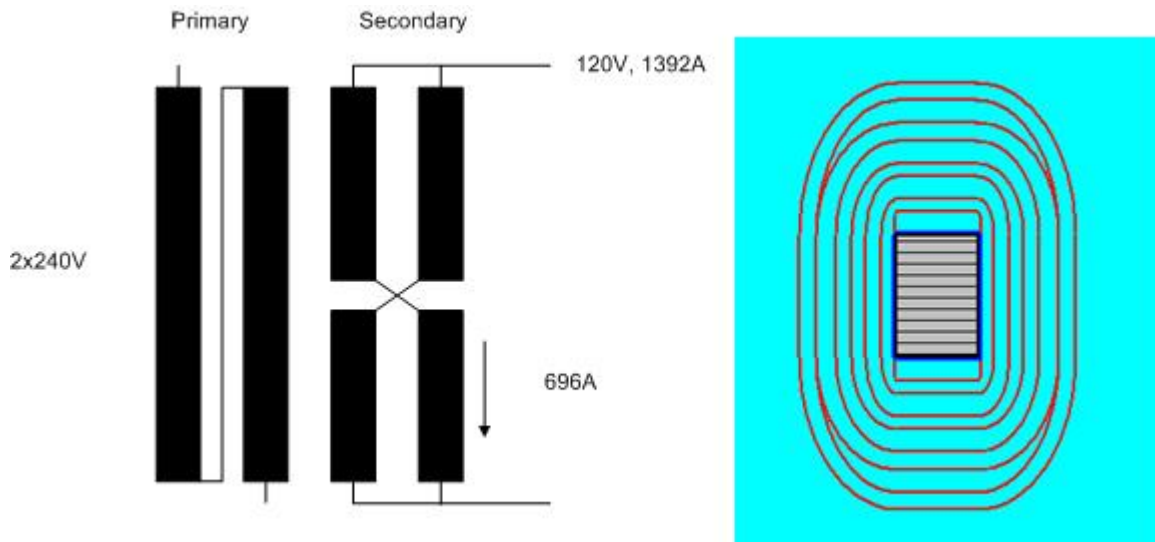
There are 4 input screens to set the input parameters for the designing of a transformer:

- Winding parameters per limb
- Core
- Environment
- Other parameters

and 3 screens for selection and set up of material :

- wires
- steels
- cores.

Windings parameters per limb



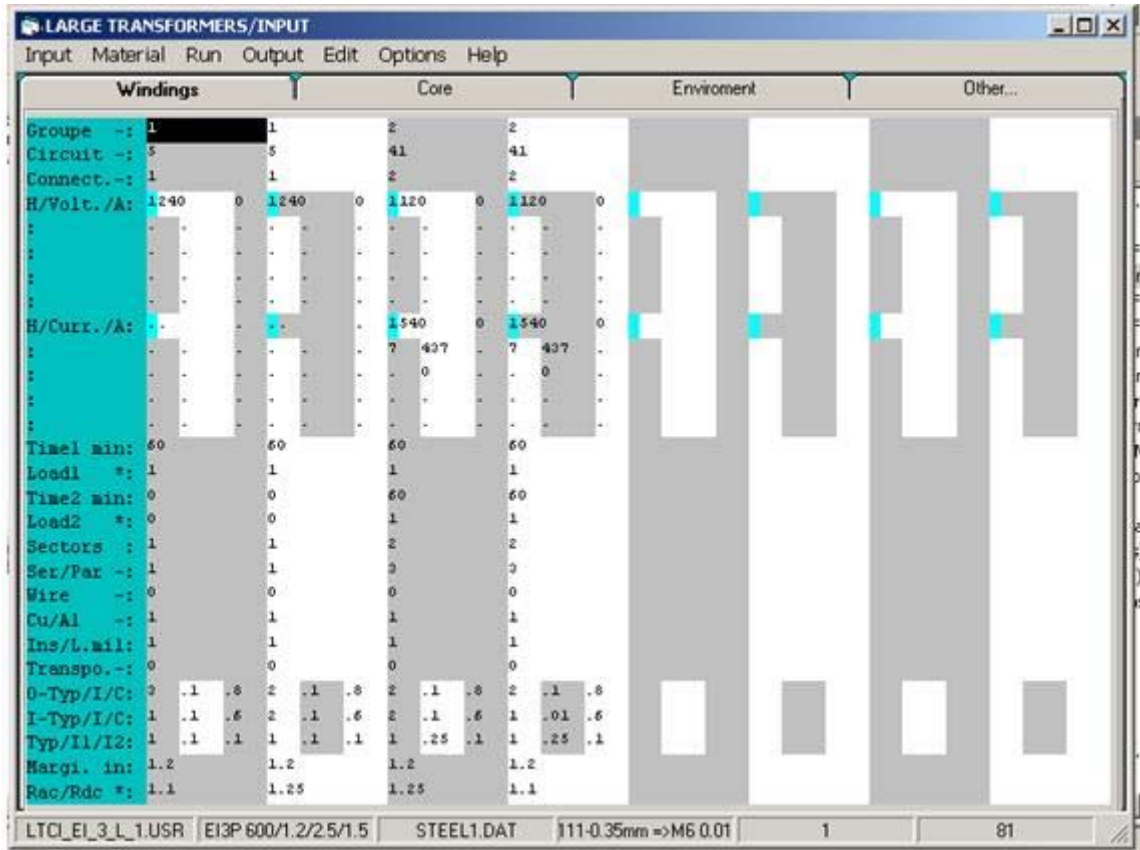
Primary

The primary is created with 2 windings connected in series. The sine wave input voltage is 480V (240V per winding).

There is no duty cycle operation mode and there are no sectors.

Note that a 500kVA transformer for K-factor=20 and the short-circuit voltage 5% can be optimal designed and manufactured only with litz wire. The round wires within the litz are not insulated but in transposition.

The first winding has the thermal contact with the center leg of the core within the core window via 0.1" tube thickness and 0.1" air gap (stomach). All other surfaces of the primary are cooled via the cooling channels of 0.6" (inside of the core window) and 0.8" (outside of the core window). The space between the yoke and the primary windings is 1.2". With the eddy current losses factor ($R_{ac}R_{dc}$) 1.1 and 1.25 shell be limited the number of the round wires per litz.



Secondary

The secondary is created with 2 windings connected in parallel . The sine wave output voltage is 120V.

The rms current per winding is 696Arms. Normally there is no explicit information about the current harmonics in a K-factor transformers. The designer has to create a combination of the first current harmonic and 7. current harmonic in order to satisfy the following conditions:

$$I1^2 + I7^2 = I_{rms}^2$$

$$1^2 \cdot I1^2 + 7^2 \cdot I7^2 = K\text{-factor} \cdot I_{rms}^2$$

For $I_{rms} = 696\text{Arms}$ and $K\text{-factor} = 20$ the calculated current harmonics $I1$ and $I7$ are:

$$I1 = 540\text{Arms}$$

$$I7 = 437\text{Arms}$$

Also there is no duty cycle operation mode on the secondary side.

In order to avoid the circulating current between 2 parallel connected secondary windings each of them is created with 2 cross connected sectors.

Once again, a 500kVA transformer for $K\text{-factor} = 20$ and the short-circuit voltage 5% can be optimal designed and manufactured only with litz wire. With the eddy current losses factor (RacRdc) 1.1 and 1.25 the number of the round wires per litz shall be limited. Note that at this point of design you can not prescribe the wire size. You can select only the wire family which the program has to use in order to select the suitable wires for your application.

The first secondary winding is cooled via the cooling channels of 0.6" (inside of the core window) and 0.8" (outside of the core window). The second secondary winding has only two 0.8" cooling channels outside of the core window. It is better cooled than the first secondary

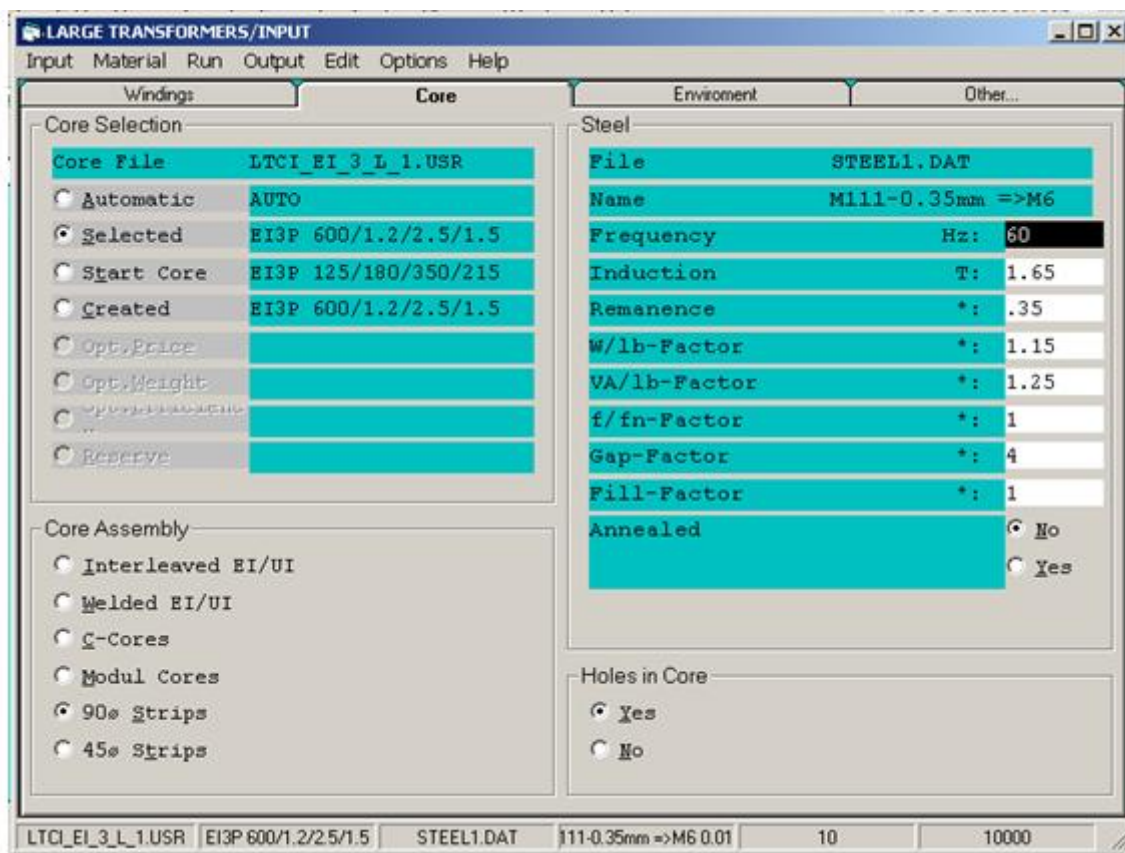
winding and therefore it is in a good thermal connection within the core window with the first secondary winding.

The space between the yoke and the secondary windings is 1.2"

Core

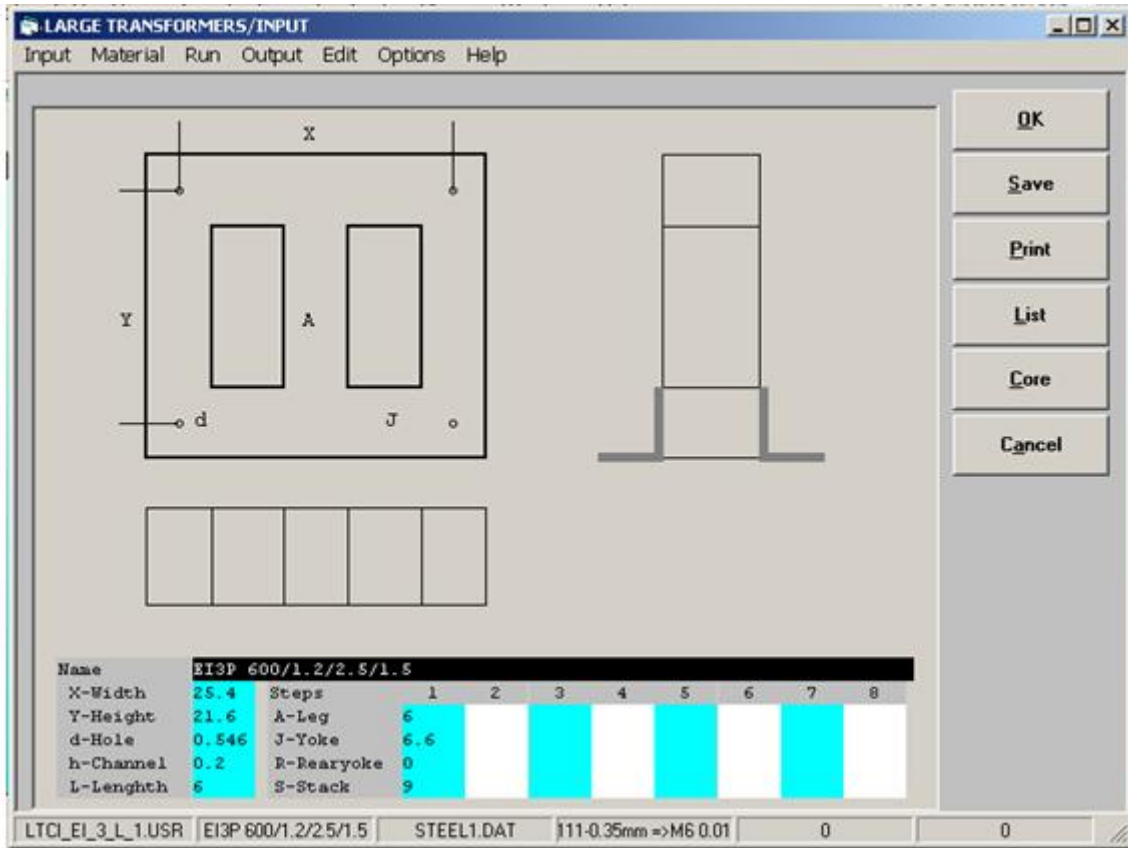
On this input screen you can :

- select and manipulate the selected steel M6, 14mil
- set the operating induction (1.65T) and the frequency (60Hz)
- select the core assembly
- and prescribe the core selection.

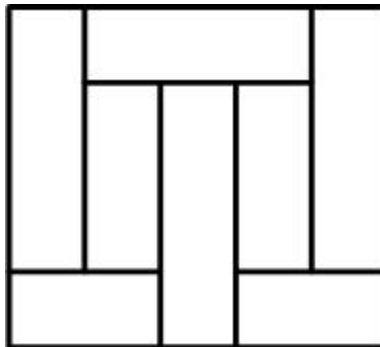


The core was created by program and by the designer in order to satisfy the following conditions:

- $U_{cc}=5\%$
- Optimal price and weight

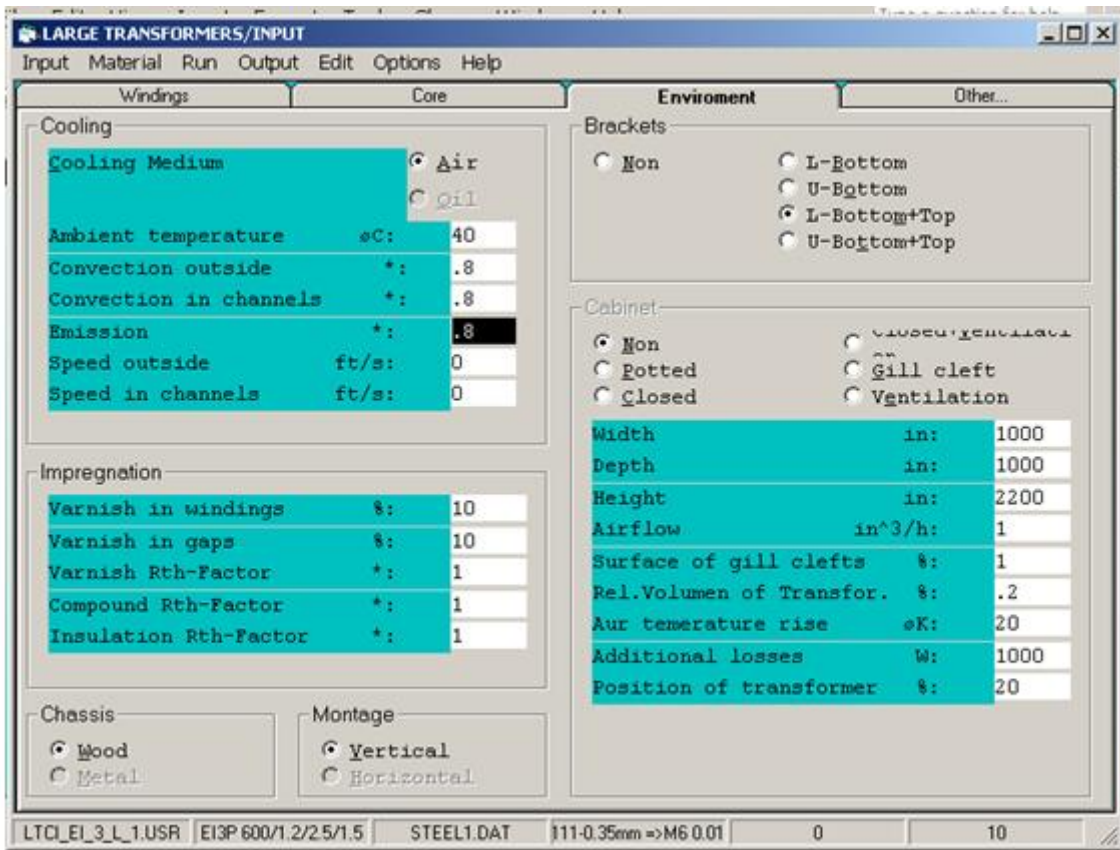


Normally for this application you use M6, 14mil, non annealed after stamping, grain oriented strips.

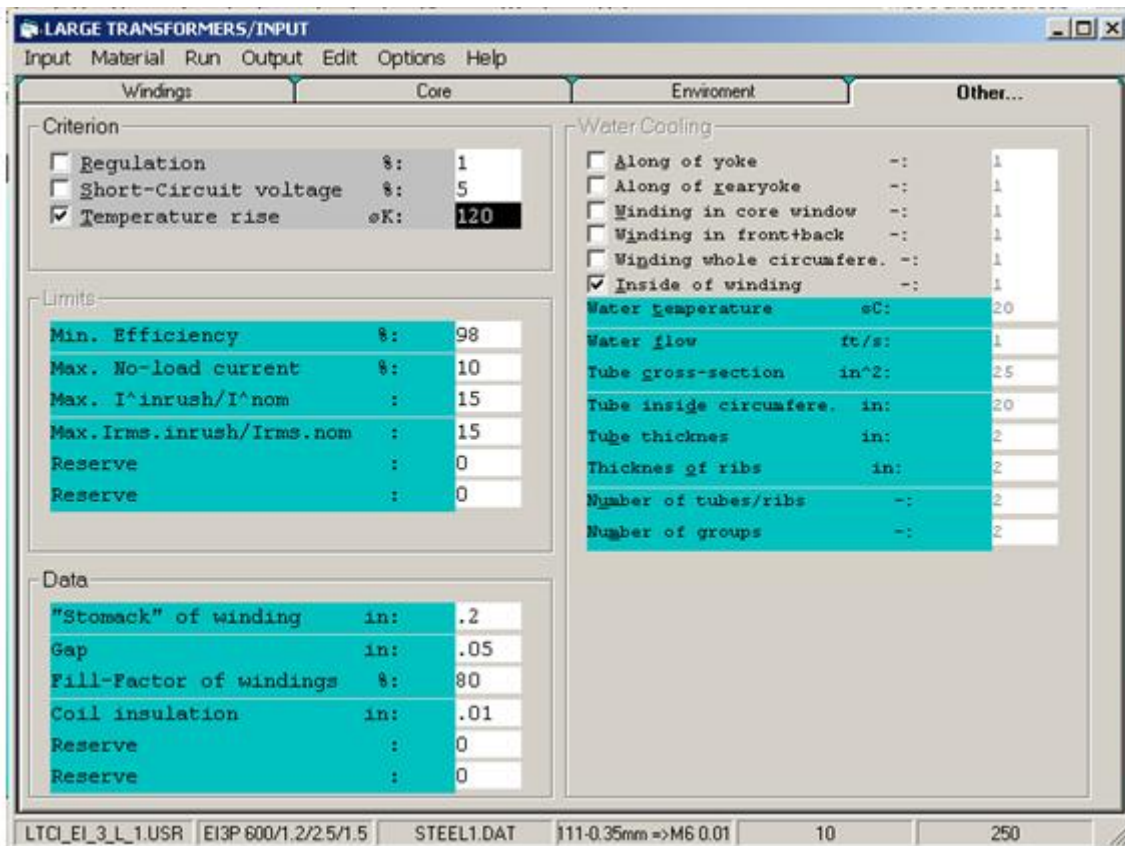


Environment

The cooling medium is air with the ambient temperature 40°C. The cooling factors for the convection and the emission are set to 80% because the transformer will be placed in a cabinet. The cooling surface of the core is increased by using 4 L-brackets on the core. The impregnation is practically "dry" because there is only 10% varnish (90% air) in the windings and in all the gaps between the insulations and the layers of the windings



Other...



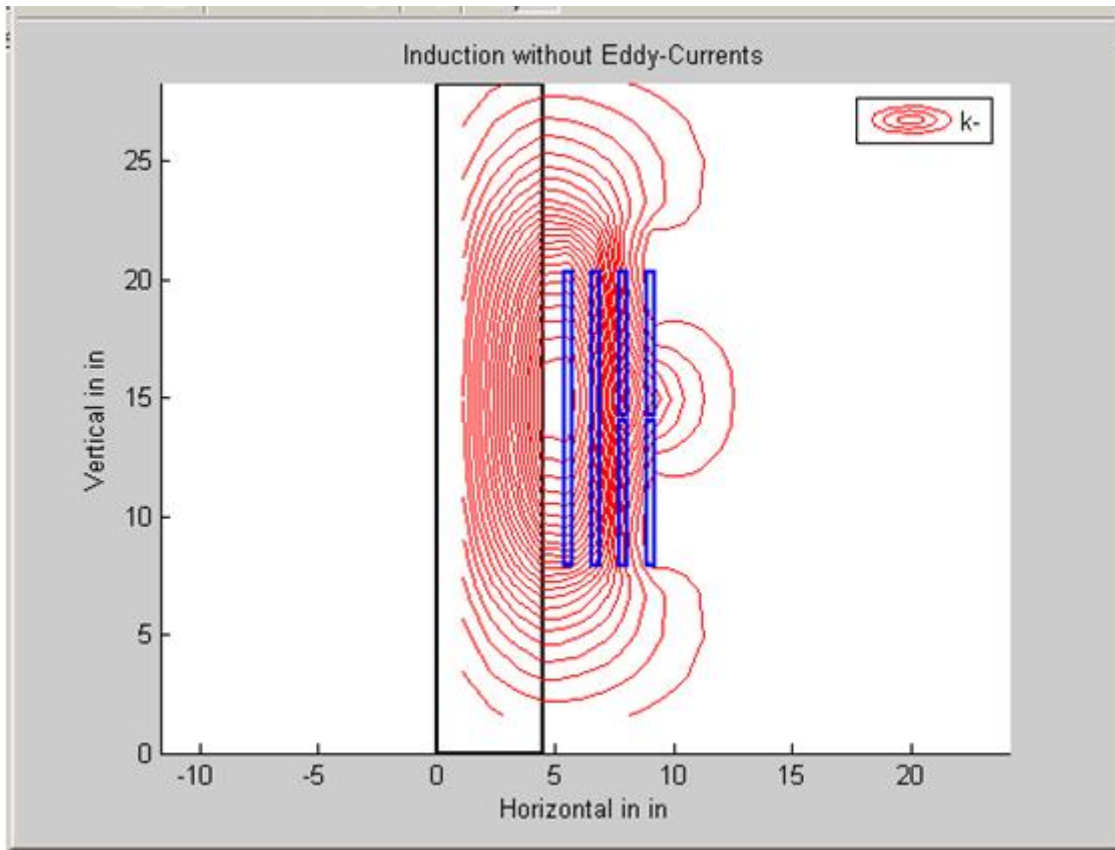
The selected criterion of the design is the temperature rise of 120°K for insulation class H. The oval space between the first winding and the tube (stomach), all gaps between the insulation, the windings and the varnish fill factor of the windings play very important roll from the thermal point of view.

Output

The first step is the presentation of the output screen DIAGNOSIS: it is the summery of the most important calculated parameters of your transformer.

DIAGNOSIS			
Name	:E13P 600/1.2/2.5/1.5		
Steel	:M111-0.35mm =>M6 0.014"		
Number of phases	-:3		
Number of legs	-:3		
Wight total/Cu/Fe	lb:2115.8	+475.1	+1'641
Max.build of windings	X:81.7		
max.wires in parrallel	:750	+50	X 15 /0
Induction on load	T:1.666		
No-load induction	T:1.674		
Max. Cu-dT on load	*K:121.2		
Max. Fe-dT on load	*K:104.8		
Regulation	X:1.264		
Short-circuit voltage cold	X:4.59	U _{cc} :4.49	U _{cr} :0.94
Efficiency	X:98.001		
Inrush/Inom max/rms	+: 10.46	7.86	
No-load current factor	X: 4.4		

Note that the program uses the numerical calculation of the magnetic fields and the temperature rises. Due to this technology the calculations of the eddy current losses, the steel losses, the short-circuit voltage, the circulating current and the transposition are very powerful. In the following picture are presented the magnetic field outside of the core window.



Finally here are 4 printed pages with all the results of the design

Input

11-11-2005/12:14:37/ U:14 13		INPUT								Page 1
	1	2	3	4	5	6	7	8		
Windings	1	2	3	4						
Groups	1	1	2	2						
Circuits	5	5	41	41						
Connection	1	1	2	2						
H/Voltage/A	1 240 0	1 240 0	1 120 0	1 120 0						
H/Current/A			1 540 0	1 540 0						
			7 437	7 437						
			0	0						
Time1 min.	60	60	60	60						
Load1	1	1	1	1						
Time2 min.	0	0	60	60						
Load2	0	0	1	1						
Sectors	1	1	2	2						
Ser./Para.	1	1	3	3						
Wire file	0	0	0	0						
Cu/Al	1	1	1	1						
In/Lay.wil	1	1	1	1						
Transpos.	0	0	0	0						
Typ/L/C in	3 0.1 0.8	2 0.1 0.8	2 0.1 0.8	2 0.1 0.8						
Typ/L/C in	1 0.1 0.6	2 0.1 0.6	2 0.1 0.6	1 0.01 0.6						
Typ/l/l in	1 0.1 0.1	1 0.1 0.1	1 0.25 0.1	1 0.25 0.1						
Margin in	1.2	1.2	1.2	1.2						
RecRdc	1.1	1.25	1.25	1.1						

Frequency	Hz: 60	Core select.	-: Selects	Cooling medium	: Air
Criterion	: dT	Core file	: LTC1_E1_3_1_	Amb. temperature	: °C: 40
Regulation	×: 1	Core name	: E130 600/1.2	Convection outside	×: 0.8
Ucc-voltage	×: 5	Core assembly	: 90° 4Strips	Convection inside	×: 0.8
Temperat. rise	°K: 120	With hole	-: No	Emission	×: 0.8
Efficiency	×: 98	Steel file	: STEEL1.DAT	Airflowoutside	ft/s: 0
No-load factor	×: 10	Steel name	: M111-0.35mm	Airflow inside	ft/s: 0
I'in/I'nom	: 15	Induction	T: 1.65	Chassis	-: Wood
I'rms/I'norms	: 15	W/lb	×: 1.15	Vertical	-: Vertical
		Wk/lb	×: 1.25	Horizontal	-: L-TAB
		Ringap	×: 4	Channel fill factor	×: 80
		f/fr-Factor	×: 1	Varnish in windings	×: 10
		Fill factor	: 1	Varnish in gaps	×: 10
		Annealed	-: No	Rth-varnish	×: 1
				Rth-compound	×: 1
				Rth-insulation	×: 1
				Coil insulation	in: 0.01
				Bauch	in: 0.2
				Gap	in: 0.05

Core

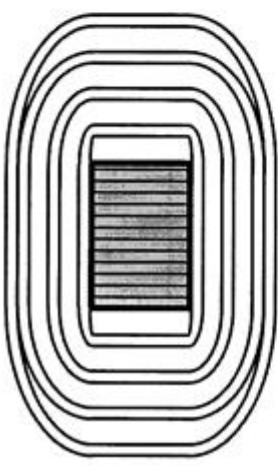
11-11-2005/12:14:37		CORE		Page 2					
Core file name : LTCI_EI_3_L_1.USR Core name : EI3P 600/1.2/2.5/1.5 Core type : 3EI Type of windings : oval/rectangular Number of legs : 3 Core assembly : 90° 8Strips Leg/Diameter in: 6 Window width in: 6.7 Window height in: 15 Stack in: 9 Cross section in^2: 52.10 Weight total lb: 1640. With holes -: Yes Brackets -: L-T&B	Fe-File name : STEEL1.DAT Fe-Name : M111-0.35mm =>M6 0.014 Frequency Hz: 60 Remanence-Factor *: 0.35 W/lb-Factor *: 1.15 UAr/lb-Factor *: 1.25 Gap-Factor *: 4 f/fn-Factor *: 1 Fillfactor *: 1 Annealed -: No Chassis -: Vertical/Horizontal-:								
	Stufen	1	2	3	4	5	6	7	8
X-Width in: 25.40	A-Leg in:6	0	0	0	0	0	0	0	0
Y-Height in: 21.6	J-Yoke in:6.6	0	0	0	0	0	0	0	0
d_Hole in: 0.546	R-Rearyoke in:0	0	0	0	0	0	0	0	0
h-Distance in: 0.2	S-Stack in:9	0	0	0	0	0	0	0	0
L-Laenght in: 6	Number lamin. :								
	Weight lb:								

Top view diagram of a magnetic core. It shows a rectangular frame with two vertical legs. Dimension X is the total width, Y is the total height, d is the hole diameter, A is the leg width, and J is the yoke width.

Side view diagram of the magnetic core, showing the vertical profile of the legs and yoke.

Bottom view diagram of the magnetic core, showing the arrangement of 8 strips used for assembly.

Windings

11-11-2005/12:14:37		WINDINGS				Page 3			
Windings		1	2	3	4	5	6	7	8
Groups-Circuits		1-D	1-D	2-Yn	2-Yn				
Connection		ser.	ser.	par.	par.				
Turns		16.0	16.0	8.0	8.0				
Build	%	13.64	42.20	70.77	81.73				
Weight	lb	33.8	40.5	39.3	44.8				
WIRE									
Type		round	round	round	round				
Thicknes	mil	22.60	22.60	22.60	22.60				
Width	mil	22.60	22.60	22.60	22.60				
WG-thicknes		23	23	23	23				
WG-width		23	23	23	23				
Al/Cu		Cu	Cu	Cu	Cu				
STRANT/LITZ									
Thickne insula.	mil	357.00	357.00	357.00	357.00			7	
Width insulata.	mil	714.0	714.0	1190.0	1190.0				
Parallel wires		450	450	750	750				
side by side		30	30	50	50				
one upon the other		15	15	15	15				
Transposition		0	0	0	0				
Cross section	mil ²	180598.	180598.	300997.	300997.				
SECTOR									
Number		1	1	2	2				
Serie/Parallel		ser.	ser.	mixed	mixed				
Turns		16	16	4	4				
Turns/Layer		16.01	16.01	4.002	4.002				
Layers		0.998	0.998	0.999	0.999				
Insul./Layer	mil	1.0	1.0	1.0	1.0				
Transposition		0	0	1	1				
Thicknes	in	0.357	0.357	0.357	0.357				
Width	in	12.40	12.40	6.075	6.075				
Distance/Sector	in	0.1	0.1	0.25	0.25				
SPACES/CHANNELS/INS.									
Outside	in	WICW	WCW	WCW	WCW				
Insulation	in	0.1	0.1	0.1	0.1				
Channel	in	0.8	0.8	0.	0.8				
Inside	in	WIW	WCW	WCW	WIW				
Insulation	in	0.1	0.1	0.1	0.01				
Channel	in	0.6	0.6	0.6	0.6				
Between sectors	in	WIW	WIW	WIW	WIW				
Distance	in	0.1	0.1	0.25	0.25				
Top/Bottom	in	0.1	0.1	0.1	0.1				
Distance to yoke	in	1.3	1.3	1.3	1.3				
<p>Coil insulation in: 0.</p> <p>D1i/D1e: 11.35 12.07</p> <p>D2i/D2e: 13.67 14.38</p> <p>D3i/D3e: 15.98 16.7</p> <p>D4i/D4e: 18.3/ 19.01</p> <p>D5i/D5e: /</p> <p>D6i/D6e: /</p> <p>D7i/D7e: /</p> <p>D8i/D8e: /</p>									
									

Nominal operating mode

11-11-2005/12:14:37		IN OPERATION MODE				Page 4		
Frequency	Hz: 60	Ventilation outsi. ft/s:	0		Fillfactor/channels	∅: 80		
Ambient temperature	C: 40	Ventilation(chann. ft/s):	0		Uarnish in windings	∅: 10		
Convection outside	*: 0.8	Rth-Insulation	*: 1		Uarnish in gaps	∅: 10		
Convection/channels	*: 0.8	Rth-Uarnish	*: 1		Stomack	in: 0.20		
Emission	*: 0.8	Rth-Epoxy	*: 1		Gap	in: 0.05		
Output power	kVA: 488.3	Input power	kVA: 499.0		Core power	: 0.0		
Fe-Losses	UA: 21062	Fe-active losses	W: 2489.		Fe-reactive losses UA:	20914		
Mo-load curren	∅: 4.4	No load curr. active	∅: 0.5		No load curr. react. ∅:	4.4		
I^in/I^nom-Factor	: 10.46	Iinrms/Inomrms-Factor	: 7.86		No load induction T:	1.674		
I^in	kA: 8.87	Iin rms	kA: 4.72		Iccx reactive cold kA:	7.40		
Icc cold	kA: 7.56	Iccr active cold	kA: 1.54		Uccx inductive cold ∅:	4.49		
Ucc cold	∅: 4.59	Uccr active cold	∅: 0.94		Efficiency	∅: 98.001		
CuAl-losses	W: 7447.0	Efficiency	∅: 98.001		Induction	T: 1.666		
Max. dT Cu/Al	*K: 121.2	Max. dT Fe	*K: 104.8					
Windings	1	2	3	4	5	6	7	8
Groups-Circuits	1-D	1-D	2-Yn	2-Yn				
Connection	ser.	ser.	par.	par.				
Time1	60.0	60.0	60.0	60.0				
Load1	1.00	1.00	1.00	1.00				
Time2	0.0	0.0	60.0	60.0				
Load2	0.00	0.00	1.00	1.00				
Voltage rms	U 239.8	240.1	118.5	118.5				
U-Phasen delay	° 0.356	-0.35	-1.70	-2.22				
Mo-load voltage	U 239.9	240.0	120.0	120.0				
Regulation	∅ 0.0	0.0	1.2	1.3				
Current rms	A 346.53	346.53	685.37	687.37				
K-Factor	20.00	20.00	20.00	20.00				
Power	kVA 83.11	83.22	81.28	81.48				
I-Phase delay	° -5.4	-4.7	-0.5	0.5				
Resistance cold mOhm	2.245	2.688	0.939	1.073				
Losses warm	W 419.5	527.7	744.3	790.6				
RacRdc (total)	1.02	1.07	1.08	1.02				
Icc.all cold	kA 7.56	7.56	15.05	15.18				
Icc.group cold	kA 0.00	0.00	15.05	15.18				
Circ.losses	W 0.00	0.00	0.00	0.00				
Cur.density A/in^2	1915.7	1915.7	2276.6	2276.6				
SECTORS								
1 RacRdc	1.02	1.07	1.07	1.02				
Current	A 346.5	346.5	685.3	687.3				
dT	*K 114.5	113.4	120.9	114.2				
2 RacRdc			1.08	1.02				
Current	A		687.37	685.37				
dT	*K		121.2	113.9				
3 RacRdc								
Current	A							
dT	*K							
4 RacRdc								
Current	A							
dT	*K							
5 RacRdc								
Current	A							
dT	*K							
6 RacRdc								
Current	A							
dT	*K							
7 RacRdc								
Current	A							
dT	*K							
8 RacRdc								
Current	A							
dT	*K							

Test Mode

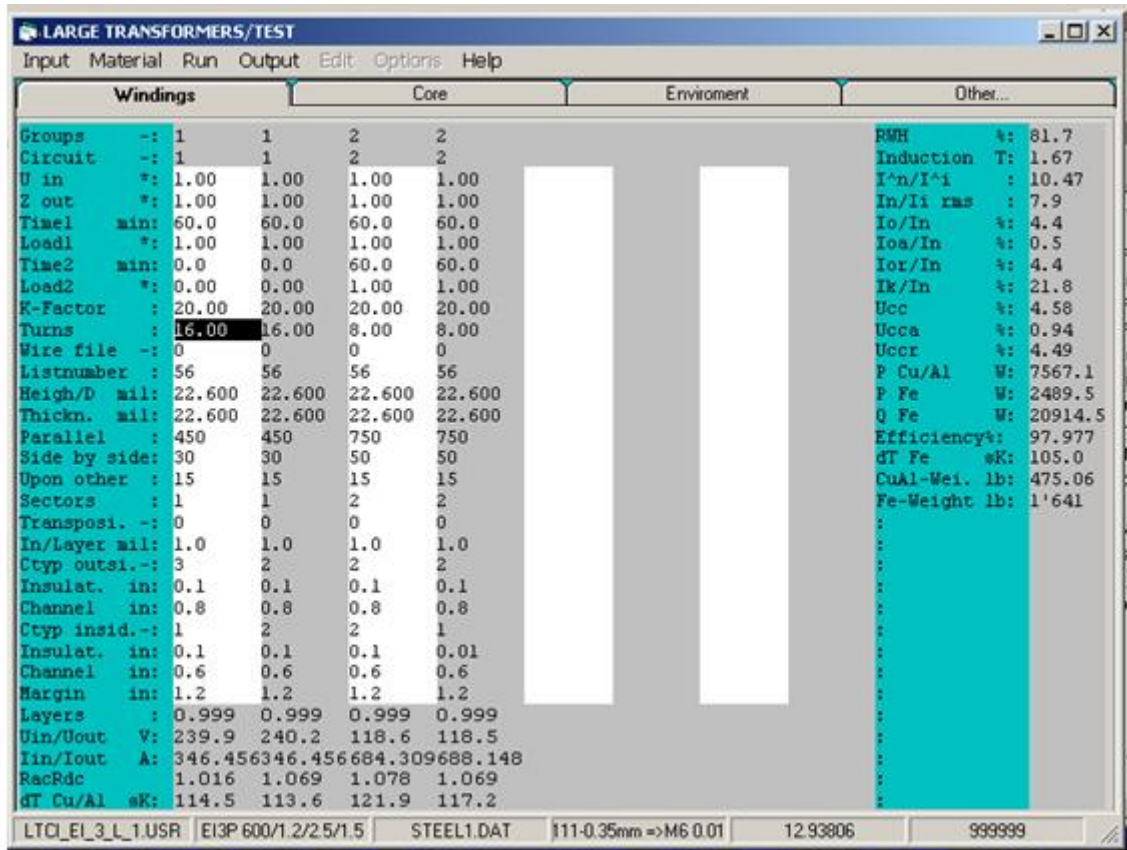
If you are not satisfied with the solution made by the program you can switch into the Test Mode and change your transformer manually:

- Turns
- Wire size
- Material (Cu or Al)
- Number parallel connected wires and their order in strand
- Cooling channels and insulations
- Margin
- Steel
- Technology parameter (impregnation, gaps,...)

and then you can set it under an operation mode changing:

- Input voltage
- Frequency
- Loads and their K-factors
- Duty cycle of each winding
- Ambient temperature
- Air flow

Note that the program could not create full layer windings at the prescribed temperature rise of 120°K. In order to get the full layer windings you have to select the wire size in the litz and the number in parallel connected wires manually.



Let us now change some technology parameters of this transformer:

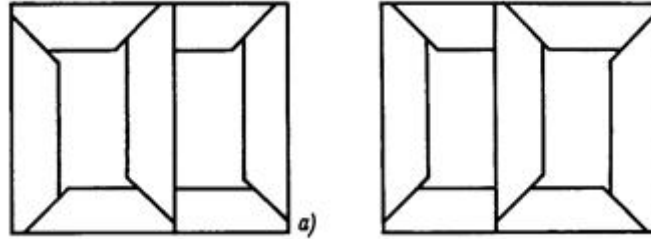
Impregnation

In the following table you can compare the temperature rise of our "dry" transformer and the full impregnated (no air in the windings, the gaps and the stomach) version.

	Core °K	Primary1 °K	Primary2 °K	Secondary1 °K	Secondary2 °K
Current version: 10% varnish	105	114	113	121	117
New version: 100% varnish	105	109	109	113	109

Core assembly

If you want to use 45° core assembly with the annealed M6 strips then:



	Core °K	Primary1 °K	Primary2 °K	Secondary1 °K	Secondary2 °K
Current version: 90° core assembly, non annealed strips	105	114	113	121	117
New version: 45° core assembly, annealed strips	90	107	109	120	116

Impregnation

In the following table you can compare the temperature rise of our "dry" transformer and the full impregnated (no air in the windings, the gaps and the stomach) version.

	Core °K	Primary1 °K	Primary2 °K	Secondary1 °K	Secondary2 °K
Current version: in the cabinet	105	114	113	121	117
New version: no cabinet	96	104	104	109	103